

GENERATION OF SH-TYPE WAVES IN LAYERED ANISOTROPIC ELASTIC MEDIA

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ABSTRACT. A study is made of the generation of SH-type waves at the free surface of a layered anisotropic elastic medium due to an impulsive stress discontinuity moving with uniform velocity along the interface of the layered medium. The exact solution for the displacement function is obtained by the Laplace and Fourier transforms combined with the modified Cagniard method. The numerical results for an important special case at two different distances are shown graphically. The results of the present study are found to be in excellent agreement with those of isotropic elastic media.

KEY WORDS AND PHRASES. SH-type waves, anisotropic elastic waves, seismology and shearing stress discontinuity.

1980 Mathematics Subject Classification Code: 73D15, 73D20, 73D30.

1. INTRODUCTION.

In recent years an attention has been given to problems of generation and propagation of waves in anisotropic or inhomogeneous elastic solids. The solutions of these problems in various geometrical configurations, and in layered media are important in geophysics, seismology, acoustics and electromagnetism. Available information strongly suggests that layered media, crystals, and various new materials such as reinforced plastics, fibre-reinforced metals, and composite materials are essentially anisotropic and/or inhomogeneous in nature. Naturally, there is a growing need for elastodynamical analysis of anisotropic and/or inhomogeneous problems in elastic materials.

Some recent works on the generation and propagation of waves in layered isotropic or anisotropic elastic media may be relevant to mention with a brief description in order to indicate our motivation. Anderson [1] made an interesting study of elastic wave propagation in layered anisotropic media with applications. He discussed the period equations for waves of Rayleigh, Stoneley, and Love types. It was shown that anisotropy can have a pronounced effect on both the range of existence and the shape of the dispersion curves. Finally, the single layer solutions in an anisotropic medium were generalized to n-layer media by the use of Haskell matrices.

Elastic properties are generally anisotropic (transversely isotropic) in sedimentary layers. Studies of Uhring and Van Melle [2], and Anderson and Harkrider [3] have indicated that anisotropy is also present in the near surface layers, and in the crust and upper mantle regions of the earth. It has been observed that the transition region between the crust and mantle is not a single layer but is possibly formed by a set of thin layers. Nag [4] made an investigation of the generation of SH-type waves at the free surface of an isotropic elastic layered medium due to an impulsive stress discontinuity moving with constant velocity after creation along the interface of the medium. In a subsequent paper Nag and Pal [5]

solved a problem similar to that of Nag with a shearing stress discontinuity at the interface of two layers of finite thickness overlying a semi-infinite medium of different elastic constants. Mention may also be made of the work on forced vibrations of an anisotropic elastic spherical shell due to an uniformly distributed internal and external pressure by Sheehan and Debnath [6].

The purpose of this paper is to study the generation of SH-type waves at the free surface of a layered anisotropic elastic medium due to an impulsive stress discontinuity moving with uniform velocity along the interface of the layered medium. The displacement function is obtained for two different types of discontinuity in the shearing stress. The numerical solution for one case at two different distances is shown graphically. Some special cases of physical interest are examined.

2. MATHEMATICAL FORMULATION OF THE PROBLEM.

We consider an anisotropic elastic layer of thickness h with elastic constants L_1, N_1 and ρ_1 over an anisotropic half-space with constants L_2, N_2 and ρ_2 . The geometrical configuration of the anisotropic wave problem is depicted in Figure 1. With the z -axis directed vertically downwards, the transversely isotropic layered structure is referred to a rectangular Cartesian coordinate system with the origin at the interface ($z=0$) of the layers I and II as shown in Figure 1. The wave generating mechanism is a shearing stress discontinuity which occurs suddenly at the interface and then moves with constant velocity V in the positive x -direction along the interface. Since only the SH-type waves are considered, we can assume that the displacement fields $u=w=0$ and v is a function of space variable x, z and t .

Neglecting body forces and assuming small deformations, the equations of motion in the two layers can be written, with the usual notations, in the form

$$\rho_i \frac{\partial^2 v_i}{\partial t^2} = N_i \frac{\partial^2 v_i}{\partial x^2} + L_i \frac{\partial^2 v_i}{\partial z^2}, \quad t > 0, \quad (2.1ab)$$

where $i = 1, 2$, v_1 and v_2 represent the displacement functions in the layers I and II respectively.

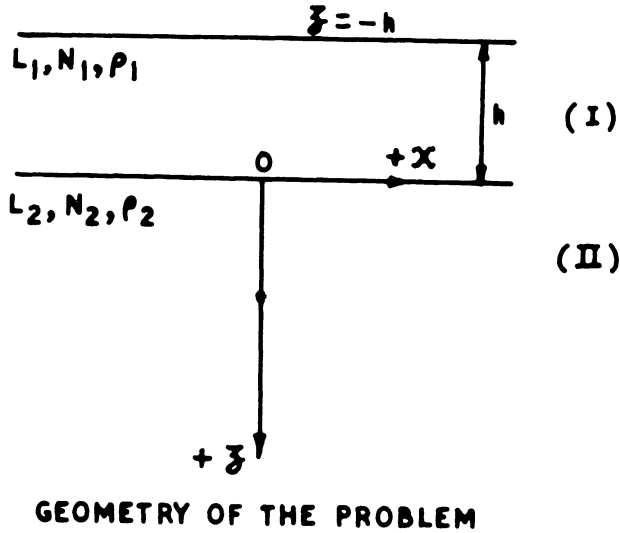


FIG. 1.

The boundary conditions are, in the usual notations,

$$(\widehat{yz})_1 = 0 \text{ at } z = -h, \ t > 0 \tag{2.2}$$

$$v_1 = v_2 \text{ at } z = 0, \ t > 0 \tag{2.3}$$

$$(\widehat{yz})_1 - (\widehat{yz})_2 = S(x,t) H(t) \text{ at } z = 0 \tag{2.4}$$

where $S(x,t)$ is a function of x and t ; $H(t)$ is the Heaviside unit function of time t , and the shearing stress in an anisotropic medium is given by

$$(\widehat{yz})_i = L_i \frac{\partial v_i}{\partial z}, \ i = 1, 2 \tag{2.5ab}$$

We complete the formulation of the problem by assuming the appropriate initial conditions and the existence of the Laplace and Fourier transforms of the functions $v_i(x,z;t)$ with respect to time t and distance x respectively.

3. THE SOLUTION OF THE PROBLEM.

The above problem can readily be solved by using the Laplace and Fourier transforms combined with the modified Cagniard method. The Laplace transform with respect to t and the Fourier transform with respect to x are defined by

$$\tilde{\bar{v}}(\xi, z; p) = \int_{-\infty}^{\infty} e^{-i\xi x} dx \int_0^{\infty} e^{-pt} v(x, z; t) dt, \tag{3.1}$$

where the tilda and the bar denote the Laplace and the Fourier transforms respectively.

Application of the double transforms (3.1) to equations (2.1ab) give the solutions in the upper and lower layers with $v_2 \rightarrow 0$ as $z \rightarrow \infty$ in the form

$$\bar{v}_1(x, z; p) = \int_{-\infty}^{\infty} (A \cosh \eta_{s1} z + B \sinh \eta_{s1} z) e^{i\xi x} d\xi, \tag{3.2}$$

$$\bar{v}_2(x, z; p) = \int_{-\infty}^{\infty} C \exp(i\xi x - \eta_{s2} z) d\xi, \tag{3.3}$$

where the constants A, B and C are to be determined from the boundary conditions (2.2) - (2.4);

$$\eta_{si} = (p^2 / \beta_{1i}^2 + \xi^2 \phi_i^2)^{\frac{1}{2}}, \quad i = 1, 2, \tag{3.4ab}$$

$$\beta_{1i} = \left(\frac{L_i}{\rho_i}\right)^{\frac{1}{2}}, \quad \beta_{2i} = \left(\frac{N_i}{\rho_i}\right)^{\frac{1}{2}}, \tag{3.5ab}$$

and $\phi_i = \beta_{2i} / \beta_{1i}$ is the anisotropic parameter for the two layers I and II.

It follows from the boundary conditions (2.2) - (2.3) that

$$A = C, \quad B \cosh \eta_{s1} h = A \sinh \eta_{s1} h, \tag{3.6ab}$$

We now consider two different forms of the functions $S(x, t)$.

$$\left. \begin{aligned} \text{Case (1): } S(x, t) &= P, \quad a \leq x \leq b + Vt \\ &= 0, \quad \text{elsewhere} \end{aligned} \right\} \tag{3.7}$$

where P is a constant.

This case implies that the stress discontinuity is created in the region $x = a$

to $x = b$ and then expands with constant velocity V in the x -direction. In particular, when $a = b = 0$, the discontinuity is created at the origin and then expands with uniform velocity V in the x -direction. When the disturbance expands in both directions after creation, this solution is to be added to the solution for negative values of x .

It follows from the transformed boundary condition (2.4) combined with (3.7) that

$$BL_1 \eta_{s1} + CL_2 \eta_{s2} = \frac{P}{2\pi p} \left[\frac{e^{-i\xi a} - e^{-i\xi b}}{i\xi} + \frac{e^{-i\xi b}}{i\xi + p/V} \right], \quad (3.8)$$

With the aid of (3.6ab) and (3.8), we solve for the three constants A, B, C ; and then write down the integral solution for the displacement function at the free surface $z = -h$ in the form

$$\begin{aligned} \bar{v}_1(x, -h, p) &= \frac{P}{2\pi p} \int_{-\infty}^{\infty} \frac{\exp(i\xi x)}{(L_1 \eta_{s1} \sinh \eta_{s1} h + L_2 \eta_{s2} \cosh \eta_{s1} h)} \times \\ &\times \left[\frac{e^{-i\xi x} - e^{-i\xi b}}{i\xi} + \frac{e^{-i\xi b}}{i\xi + p/V} \right] d\xi \\ &= \frac{P}{\pi p} \int_{-\infty}^{\infty} \frac{\exp(i\xi x - h\eta_{s1})}{(L_1 \eta_{s1} + L_2 \eta_{s2})} \left[\frac{e^{-i\xi a} - e^{-i\xi b}}{i\xi} + \frac{e^{-i\xi b}}{i\xi + p/V} \right] \left(1 - Ke^{-2h\eta_{s1}}\right)^{-1} d\xi, \end{aligned} \quad (3.9)$$

where $K(<1)$ represents the reflection parameter given by

$$K = \frac{L_1 \eta_{s1} - L_2 \eta_{s2}}{L_1 \eta_{s1} + L_2 \eta_{s2}} \quad (3.10)$$

Using the inverse Laplace transform, we can rewrite (3.9) in a convenient form

$$v_1(x, -h; p) = L^{-1}(I_1 + I_2 + I_3), \quad (3.11)$$

where L^{-1} stands for the inverse Laplace transform and

$$I_1 = \frac{P}{\pi p} \int_{-\infty}^{\infty} \frac{\left(1 - Ke^{-2h\eta_{s1}}\right)^{-1}}{i\xi(L_1 \eta_{s1} + L_2 \eta_{s2})} \exp(i\xi x_1 - h\eta_{s1}) d\xi, \quad (3.12)$$

$$I_2 = \frac{P}{\pi p} \int_{-\infty}^{\infty} \frac{(1 - Ke^{-2h\eta_{s1}})^{-1}}{i\xi(L_1\eta_{s1} + L_2\eta_{s2})} \exp(i\xi x_2 - h\eta_{s1}) d\xi, \tag{3.13}$$

$$I_3 = \frac{P}{\pi p} \int_{-\infty}^{\infty} \frac{(1 - Ke^{-2h\eta_{s1}})^{-1}}{(i\xi + p/V)(L_1\eta_{s1} + L_2\eta_{s2})} \exp(i\xi x_2 - h\eta_{s1}) d\xi, \tag{3.14}$$

with $x_1 = x - a$ and $x_2 = x - b$.

In order to evaluate the Laplace inversion integral, we shall use the modified Cagniard method due to Garvin [7] who discussed the contour integration and mapping in detail. It may be fair to avoid duplication of mathematical analysis similar to that of Garvin, and to quote some necessary results from that paper without proof.

We next substitute $\xi = p\zeta/\beta_{11}$ in (3.4ab) and 3.10) so that

$$\eta_{s1} = \frac{p}{\beta_{11}} (1 + \zeta^2 \phi_1^2)^{\frac{1}{2}}, \quad \eta_{s2} = \frac{p}{\beta_{11}} \left(\frac{\beta_{11}^2}{\beta_{12}^2} + \zeta^2 \phi_2^2 \right)^{\frac{1}{2}}, \tag{3.15ab}$$

and

$$K = \frac{L_1(1 + \zeta^2 \phi_1^2)^{\frac{1}{2}} - L_2 \left(\frac{\beta_{11}^2}{\beta_{12}^2} + \zeta^2 \phi_2^2 \right)^{\frac{1}{2}}}{L_1(1 + \zeta^2 \phi_1^2)^{\frac{1}{2}} + L_2 \left(\frac{\beta_{11}^2}{\beta_{12}^2} + \zeta^2 \phi_2^2 \right)^{\frac{1}{2}}}, \tag{3.16}$$

We thus obtain

$$I_1 = \frac{2P}{\pi p} \operatorname{Im} \int_0^{\infty} \frac{\exp(i\xi x_1 - h\eta_{s1})}{\xi(L_1\eta_{s1} + L_2\eta_{s2})} (1 + Ke^{-2h\eta_{s1}} + K^2 e^{-4h\eta_{s1}} + \dots) d\xi, \tag{3.17}$$

where η_{s1} and η_{s2} are given by (3.15ab).

Denoting the first term of I , in (3.17) by I_{11} , we get

$$I_{11} = \frac{2P}{\pi p^2 \rho_1 \beta_{11}} \operatorname{Im} \int_0^{\infty} \frac{\exp \left[-p \left\{ -i\zeta x_1 + h(1 + \zeta^2 \phi_1^2)^{\frac{1}{2}} \right\} \div \beta_{11} \right] d\zeta}{\zeta \left[(1 + \zeta^2 \phi_1^2)^{\frac{1}{2}} + \frac{L_2}{L_1} \left(\frac{\beta_{11}^2}{\beta_{12}^2} + \zeta^2 \phi_2^2 \right)^{\frac{1}{2}} \right]} \tag{3.18}$$

The integrand of (3.18) has singularities at $\zeta = 0, \pm 1/\phi_1$ and $\pm i \beta_{11}/\phi_2 \beta_{12}$. Setting

$$t = [-i\zeta x_1 + h(1 + \zeta^2 \phi_1^2)^{\frac{1}{2}}] \beta_{11}^{-1}, \quad (3.19)$$

so that the inversion gives

$$\zeta(t) = \frac{\beta_{11}}{(x_1^2 + h^2 \phi_1^2)^{\frac{1}{2}}} [itx_1 + h\{t^2 - (x_1^2 + h^2 \phi_1^2) \beta_{11}^{-2}\}^{\frac{1}{2}}], \quad (3.20)$$

The singularities in the ζ -plane are shown in Figure 2, and the mapping and contour in the t -plane are depicted in Figure 3. Making reference to these Figures and to the paper [4], we find

$$L^{-1}I_{11} = \frac{2P}{\pi \rho_1 \beta_{11}} \int_0^t (t - \tau) G_{1,1}[\zeta_{1,1}(\tau)] d\tau, \quad (3.21)$$

where $L[tH(t)] = \frac{1}{p^2}$ and

$$G_{1,t}[\zeta(t)] = \text{Im}[\{1 + \phi_1^2 \zeta_{1,1}^2(t)\}^{\frac{1}{2}} + \frac{L_2}{L_1} \{\frac{\beta_{11}^2}{\beta_{12}^2} + \phi_2^2 \zeta_{1,1}^2(t)\}^{\frac{1}{2}}] \\ \times \zeta_{1,1}^{-1} \cdot \frac{d}{dt} \zeta_{1,1}(t) \cdot H\{t - (x_1^2 + h^2 \phi_1^2)^{\frac{1}{2}} \beta_{11}^{-1}\}, \quad (3.22)$$

Since $h\phi_1 \beta_{11}^{-1} < t < (x_1^2 + h^2 \phi_1^2)^{\frac{1}{2}} \beta_{11}^{-1}$, the expression

$$[\{1 + \zeta_{1,1}^2(t) \phi_1^2\}^{\frac{1}{2}} + \frac{L_2}{L_1} \{\frac{\beta_{11}^2}{\beta_{12}^2} + \phi_2^2 \zeta_{1,1}^2(t)\}^{\frac{1}{2}}] \text{ is real. In general, it turns}$$

out that

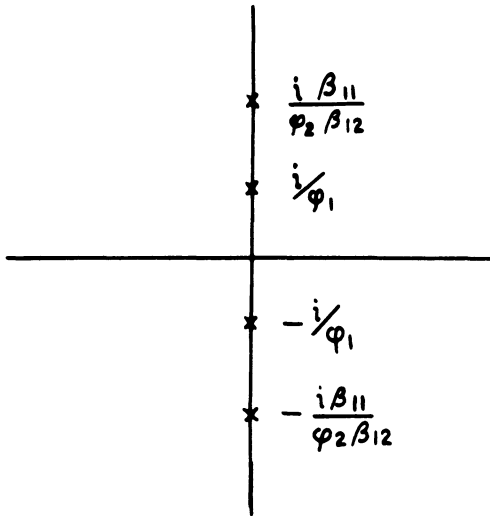
$$L^{-1}I_{1,n} = \frac{2P}{\pi \rho_1 \beta_{11}} \int_0^t (t - \tau) G_{1,n}[\zeta_{1,n}(\tau)] d\tau, \quad (3.23)$$

where

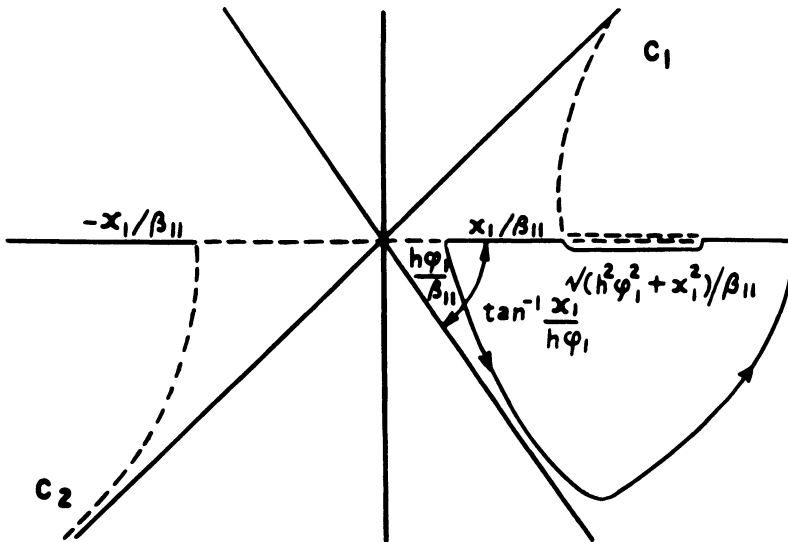
$$G_{1,n}[\zeta_{1,n}(t)] = \text{Im}[\{1 + \phi_1^2 \zeta_{1,n}^2(t)\}^{\frac{1}{2}} + \frac{L_2}{L_1} \{\frac{\beta_{11}^2}{\beta_{12}^2} + \phi_2^2 \zeta_{1,n}^2(t)\}^{\frac{1}{2}}] \\ \times \zeta_{1,n}^{-1} \frac{d}{dt} \zeta_{1,n}(t) H\{t - (x_1^2 + n^2 h^2 \phi_1^2)^{\frac{1}{2}} \beta_{11}^{-1}\}, \quad (3.24)$$

and

$$\zeta_{1,n}(t) = \frac{\beta_{11}}{(x_1^2 + n^2 h^2 \phi_1^2)^{\frac{1}{2}}} [ix_1 t + nh\{t^2 - (x_1^2 + n^2 h^2 \phi_1^2) \beta_{11}^{-2}\}^{\frac{1}{2}}], \quad n = 1, 3, 5, \dots \\ \dots, \quad (3.25)$$



z - PLANE SHOWING THE SINGULARITIES
FIG. 2.



t - PLANE SHOWING THE MAPPING AND THE CONTOUR
FIG. 3.

so that

$$L^{-1}I_1 = \sum_{n=1,3,5\dots} L^{-1}I_{1,n}, \tag{3.26}$$

Similarly, we obtain

$$L^{-1}I_2 = \sum_{n=1,3,5\dots} L^{-1}I_{2,n} \tag{3.27}$$

A similar procedure gives that

$$L^{-1}I_3 = \sum_{n=1,3,5\dots} L^{-1}I_{3,n} \tag{3.28}$$

where

$$L^{-1}I_{3,n} = \frac{2P}{\pi\rho_1\beta_{11}} \int_0^t (t - \tau)G_{3,n}[\zeta_{2,n}(\tau)]d\tau, \tag{3.29}$$

$$G_{3,n}[\zeta_{2,n}(t)] = \text{Re}[\{1 + \phi_1^2 \zeta_{2,n}^2(t)\}^{\frac{1}{2}} + \frac{L_2}{L_1} \{ \frac{\beta_{11}^2}{\beta_{12}^2} + \phi_2^2 \zeta_{2,n}^2(t) \}^{\frac{1}{2}}] \\ \times [\frac{\beta_{11}}{V} + i\zeta_{2,n}(t)]^{-1} K^{\frac{n-1}{2}} \zeta_{2,n} \frac{d \zeta_{2,n}(t)}{dt} H\{t - (x_2^2 + n^2 h^2 \phi_1^2)^{\frac{1}{2}} \beta_{11}^{-1}\}, \tag{3.30}$$

and $\zeta_{2,n}(t)$ is given by (3.25) with x_2 in place of x_1 .

Finally, a simple combination of the results (3.26) - (3.28) gives the exact value of the free surface displacement field $v_1(x, -h,t)$.

Case(ii): $S(x,t) = Ph \delta(x - Vt), \tag{3.31}$

where P is a constant, $\delta(r)$ is the Dirac distribution and a factor h is included in (3.31) so that P has the dimension of stress.

The boundary condition (2.4) given

$$BL_1\eta_{s1} + CL_2\eta_{s2} = \frac{Ph}{2\pi V(i\xi+P/V)}, \tag{3.32}$$

Solving A , B , and C from (3.6 ab) and (3.32), we obtain the solution as

$$\bar{v}_1(x, -h;p) = \frac{Ph}{\pi V} \int_{-\infty}^{\infty} \frac{(1+K e^{-2\eta_{s1}h} + \dots)}{(L_1\eta_{s1}+L_2\eta_{s2})(i\xi+P/V)} \exp(i\xi x - h\eta_{s1})d\xi \tag{3.33}$$

A procedure similar to that of Case (i) gives the solution in the form

$$v_1(x, -h, t) = \frac{2Ph}{\pi V \beta_{11}} \sum_{n=1,3,5,\dots} \int_0^t G_n[\zeta_n(\tau)] d\tau, \tag{3.34}$$

where

$$G_n[\zeta_n(t)] = \text{Re} \left\{ [1 + \phi_1^2 \zeta_n^2(t)]^{\frac{1}{2}} + \frac{L_2}{L_1} \left\{ \frac{\beta_{11}}{\beta_{12}^2} + \phi_2^2 \zeta_n^2(t) \right\}^{\frac{1}{2}} \right\} \times \\ \times \left[\frac{\beta_{11}}{V} + i \zeta_n(t) \right]^{-1} \frac{d \zeta_n(t)}{dt} K^{\frac{n-1}{2}} \zeta_n(t) H \left\{ t - (x^2 + n^2 h^2 \phi_1^2)^{\frac{1}{2}} \beta_{11}^{-1} \right\}, \tag{3.35}$$

and

$$\zeta_n(t) = \frac{\beta_{11}}{(x^2 + n^2 h^2 \phi_1^2)^{\frac{1}{2}}} [i t x + n h \{ t^2 - (x^2 + n^2 h^2 \phi_1^2) \beta_{11}^{-2} \}^{\frac{1}{2}}], \tag{3.36}$$

If the stress discontinuity is taken as $H(x) - H(x - Vt)$ in place of $\delta(x - Vt)$, the corresponding result on the right hand side of (3.33) differ only by a constant factor from I_3 (with $a = b = 0$) in (3.12) - (3.14).

4. NUMERICAL RESULTS:

It is of interest to consider the initial behavior of the displacement field $v_1(x, -h, t)$ for case (ii) numerically.

Following Nag and Pal [5], motion due to each of the pulses at the instant of their arrival has been investigated. We consider the following numerical values:

$$\phi_1 = 0.9, \phi_2 = 1.1, L_2/L_1 = 1.33, \beta_{11}/V = 1.21, \beta_{11}/\beta_{12} = 1.02.$$

The initial behavior of $v_1(x, -h, t)$ at two different distances is examined.

(1) When $x = 5h, t = \frac{\tau h}{\beta_{11}}$, for six initial values, we have

$$K_1 v_1(x, -h, t) \approx [A^0(\theta_1) \cosh^{-1} \frac{\tau}{5.2} H(\tau - 5.2) + \\ + A^0(\theta_3) \cosh^{-1} \frac{\tau}{6.3} H(\tau - 6.3) + A^0(\theta_5) \cosh^{-1} \frac{\tau}{8.2} H(\tau - 8.2) \\ + A^0(\theta_7) \cosh^{-1} \frac{\tau}{10.1} H(\tau - 10.1) + A^0(\theta_9) \cosh^{-1} \frac{\tau}{12.6} H(\tau - 12.6) + \\ + A^0(\theta_{11}) \cosh^{-1} \frac{\tau}{15.2} H(\tau - 15.2)], \tag{4.1}$$

where $K_1 = \frac{2.42 P \rho_1}{\pi \cdot \beta_{11}}$, (4.2)

and

$$A^0(\theta_n) = \text{Re} \frac{[(1-1.76\cos^2\theta_n)^{1/2} - 0.95(1.04 - 2.1\cos^2\theta_n)^{1/2}]^{\frac{n-1}{2}} \sin \theta_n}{[(1-1.76\cos^2\theta_n)^{1/2} + 0.95(1.04-2.1\cos^2\theta_n)^{1/2}]^{\frac{n-3}{2}} (1.2 - \cos\theta_n)}$$

(4.3)

$n = 1, 3, 5, \dots$

(2) When $x = 10h$, $t = \frac{\tau h}{\beta_{11}}$, for six initial values, we have

$$K_1 v_1(x, -h, t) \approx [A^0(\theta_1)\cosh^{-1} \frac{\tau}{10.08} H(\tau - 10.08) + A^0(\theta_3)\cosh^{-1} \frac{\tau}{10.71} H(\tau - 10.71) + A^0(\theta_5)\cosh^{-1} \frac{\tau}{11.94} H(\tau - 11.94) + A^0(\theta_7)\cosh^{-1} \frac{\tau}{13.64} H(\tau - 13.64) + A^0(\theta_9)\cosh^{-1} \frac{\tau}{15.5} H(\tau - 15.5) + A^0(\theta_{11})\cosh^{-1} \frac{\tau}{17.62} H(\tau - 17.62)],$$
 (4.4)

where $A^0(\theta_n)$, $n = 1, 3, 5, \dots$ are given by (4.3).

Values of $A^0(\theta_n)$, $n = 1, 3, 5, \dots$ for $x = 5h$ and $x = 10h$ are tabulated below:

TABLE 1.

$A^0(\theta_n)$	$A^0(\theta_1)$	$A^0(\theta_3)$	$A^0(\theta_5)$	$A^0(\theta_7)$	$A^0(\theta_9)$	$A^0(\theta_{11})$
$x = 5h$	0.74	-0.301	0.052	-0.122	0.0009	-0.00012
$x = 10h$	0.23	-0.02	0.0165	-0.0035	0.00055	-0.0002

5. DISCUSSION AND CONCLUSIONS.

The exact form of the displacement field due to physically realistic shearing stress discontinuity has been obtained. The value of $K_1 v_1(x, -h, t)$ for $x = 5h$ and $x = 10h$ have been plotted against $\tau_1 = \tau - \tau_0$ where τ_0 is the time at which the disturbances arrive at the point of observation. The values of for

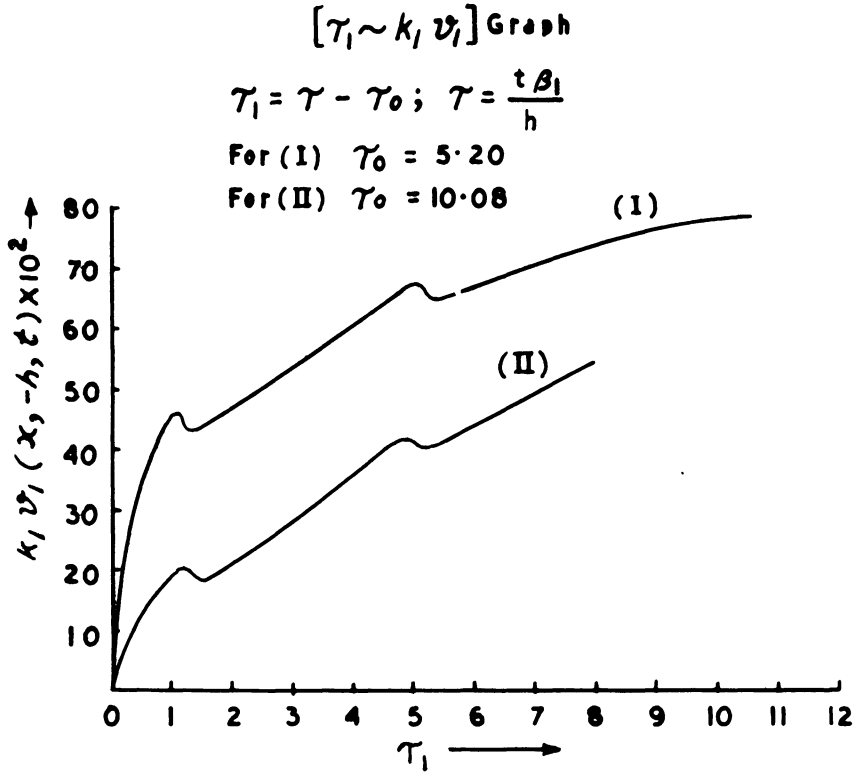


FIG. 4.

$x = 5h$ and $x = 10h$ are 5.2 and 10.08 respectively. These results are shown in Figure 4. It is clear from Figure 4 that the curves start from the origin and undergo sharp changes in their slopes with sudden jerking as the different pulses arrive after undergoing reflections from the boundaries of the anisotropic layers. These changes occur for $x = 5h$ at $\tau = (5^2 + 0.81 n^2)^{1/2}$, $n = 1, 5, 9, \dots$; and for $x = 10h$ at $\tau = (10^2 + 0.81 n^2)^{1/2}$, $n = 1, 5, 9, \dots$. We also infer that the contribution due to the third pulse for $x = 10h$ will arrive in a shorter time than for $x = 5h$.

In addition to above two special disturbances, the present analysis incorporates other forms of physically realistic stress discontinuity for the generation of SH

type waves in both isotropic and anisotropic elastic media.

In the case of the layered isotropic media, $\phi_1 = 1$, $i = 1, 2$; the results of the present analysis reduce to those of Nag [4] for the corresponding isotropic problem.

Finally the shearing stress discontinuity is always associated with the propagation of cracks in earthquakes. Hence the present study has direct applications to geophysics and seismology. In addition, the present study is of interest in connection with the propagation of cracks in sedimentary layers, and in particular in elastic layers having anisotropic property in general.

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